

Op-Amp Sallen-Key Filter Design

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The relative sensitivity of y to x is defined as

$$S_x^y = \frac{\partial y / y}{\partial x / x} = \left(\frac{\partial y}{\partial x} \right) \frac{x}{y} \quad (1)$$

and is useful for optimizing component values in filter designs. Designing for low sensitivity is a way to minimize variations in filter parameters due to component tolerances.

1 Low-Pass Filter

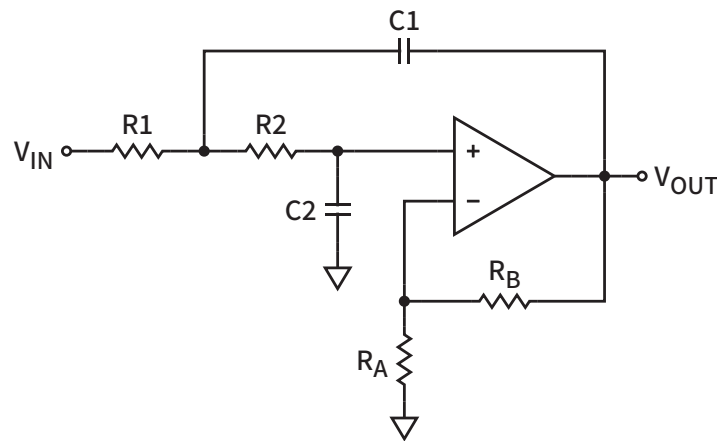


Figure 1: Sallen-Key low-pass filter schematic.

$$H(s) = H_0 \frac{1}{s^2/\omega_0^2 + s/(\omega_0 Q) + 1} \quad (2)$$

$$H_0 = K = 1 + R_B/R_A \quad (3)$$

$$\omega_0 = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}} \quad (4)$$

$$Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{(1 - K) R_1 C_1 + (R_1 + R_2) C_2} \quad (5)$$

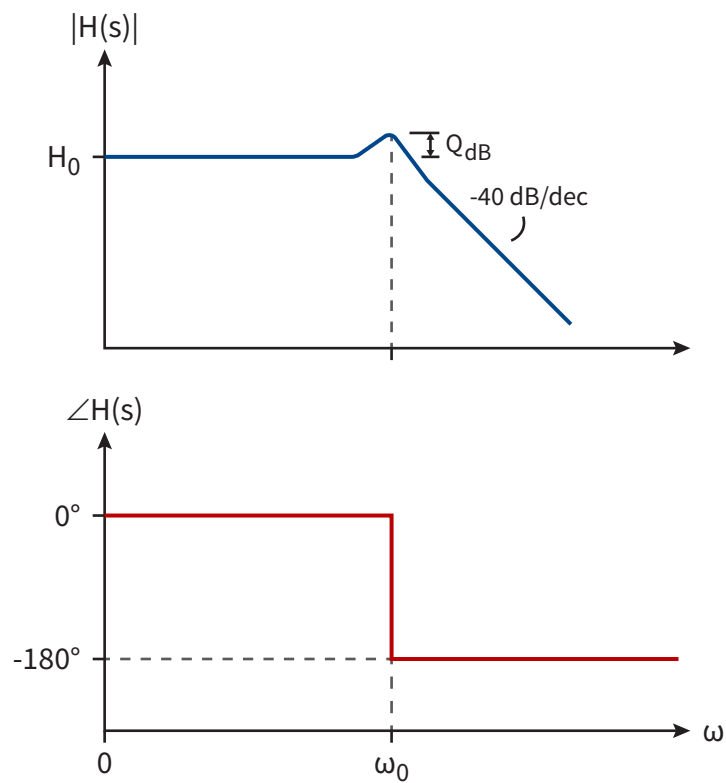


Figure 2: Sallen-Key low-pass filter Bode plot.

1.1 Sensitivity

$$S_{R_1}^{\omega_0} = S_{R_2}^{\omega_0} = S_{C_1}^{\omega_0} = S_{C_2}^{\omega_0} = -\frac{1}{2} \quad (6)$$

$$S_{R_B}^{\omega_0} = S_{R_A}^{\omega_0} = 0 \quad (7)$$

$$S_{R_1}^Q = -S_{R_2}^Q = \omega_0 Q R_2 C_2 - \frac{1}{2} \quad (8)$$

$$S_{C_1}^Q = -S_{C_2}^Q = \omega_0 Q (R_1 C_2 + R_2 C_2) - \frac{1}{2} \quad (9)$$

$$S_{R_B}^Q = -S_{R_A}^Q = \omega_0 Q (K - 1) R_1 C_1 \quad (10)$$

1.2 Components as Ratios

$$\begin{aligned} R_1 &= mR \\ R_2 &= R \\ C_1 &= nC \\ C_2 &= C \end{aligned} \quad (11)$$

$$\omega_0 = \frac{1}{RC\sqrt{mn}} \quad (12)$$

$$Q = \frac{\sqrt{mn}}{(1-K)mn + m + 1} \quad (13)$$

1.2.1 Minimizing Resistor Sensitivity

$$S_{R_1}^Q = S_{R_2}^Q = 0 \text{ for}$$

$$\omega_0 Q R_2 C_2 = \frac{1}{(1-K)mn + m + 1} = \frac{1}{2} \quad (14)$$

$$\Rightarrow n = \frac{m-1}{(K-1)m} \quad (15)$$

Substituting n into Q and solving for m ,

$$m = 1 + 4Q^2 (K - 1) \quad (16)$$

$$\Rightarrow n = \frac{4Q^2}{1 + 4Q^2 (K - 1)} \quad (17)$$

If C is chosen, then R can be calculated from ω_0 as

$$R = \frac{1}{2\omega_0 Q C} \quad (18)$$

1.2.2 Minimizing Capacitor Sensitivity

$S_{C_1}^Q = S_{C_2}^Q = 0$ for

$$\omega_0 Q (R_1 C_2 + R_2 C_2) = \frac{m + 1}{(1 - K) mn + m + 1} = \frac{1}{2} \quad (19)$$

However, the ratio expression has a minimum value of 1, so the minimum capacity sensitivity is $S_{C_1}^Q = -S_{C_2}^Q = 1/2$ and occurs when $K = 1$.

1.2.3 Monte Carlo Simulation

The circuit used to generate the plot was designed for $K = 1$, $\omega_0 = 2\pi \cdot 1000$, and $Q = 1.5$. The resistor and capacitor tolerances were set to 1% and 5%, respectively.

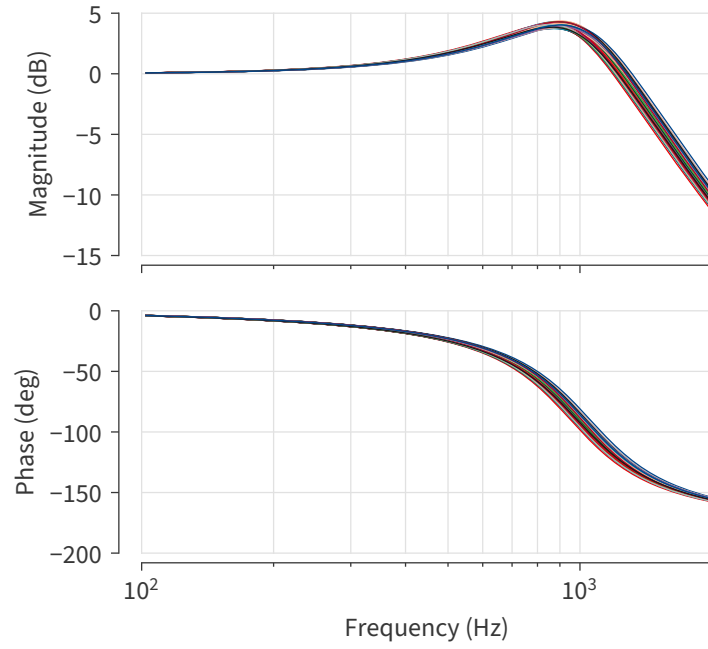


Figure 3: Sallen-Key low-pass filter Bode plot of 100 Monte Carlo samples.

1.3 Resistors as Ratios and Equal Capacitors

$$\begin{aligned}
 R_1 &= mR \\
 R_2 &= R \\
 C_1 &= C_2 = C
 \end{aligned}
 \tag{20}$$

$$\omega_0 = \frac{1}{RC\sqrt{m}}
 \tag{21}$$

$$Q = \frac{\sqrt{m}}{(2-K)m+1}
 \tag{22}$$

If C is chosen, then

$$m = \frac{4Q^2}{\left[1 + \sqrt{1 + 4Q^2(K - 2)}\right]^2} \quad (23)$$

$$R = \frac{1 + \sqrt{1 + 4Q^2(K - 2)}}{2\omega_0QC} \quad (24)$$

1.4 Equal Components

$$\begin{aligned} R_1 &= R_2 = R \\ C_1 &= C_2 = C \end{aligned} \quad (25)$$

$$\omega_0 = \frac{1}{RC} \quad (26)$$

$$Q = \frac{1}{3 - K} \quad (27)$$

2 High-Pass Filter

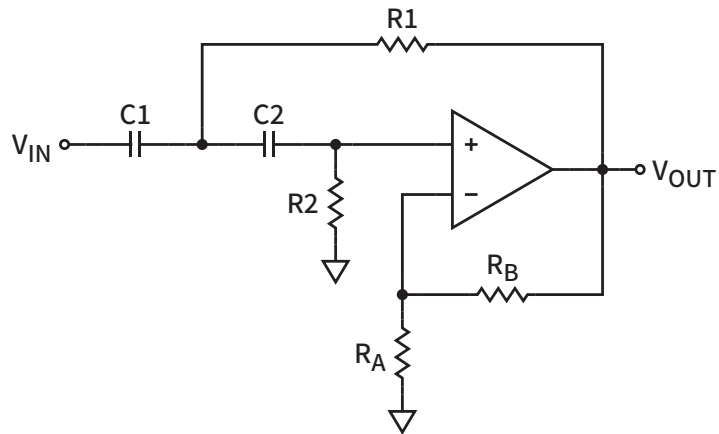


Figure 4: Sallen-Key high-pass filter schematic.

$$H(s) = H_0 \frac{s^2/\omega_0^2}{s^2/\omega_0^2 + s/(\omega_0 Q) + 1} \quad (28)$$

$$H_0 = K = 1 + R_B/R_A \quad (29)$$

$$\omega_0 = \frac{1}{\sqrt{R_1 R_2 C_1 C_2}} \quad (30)$$

$$Q = \frac{\sqrt{R_1 R_2 C_1 C_2}}{(1 - K) R_2 C_2 + R_1 (C_1 + C_2)} \quad (31)$$

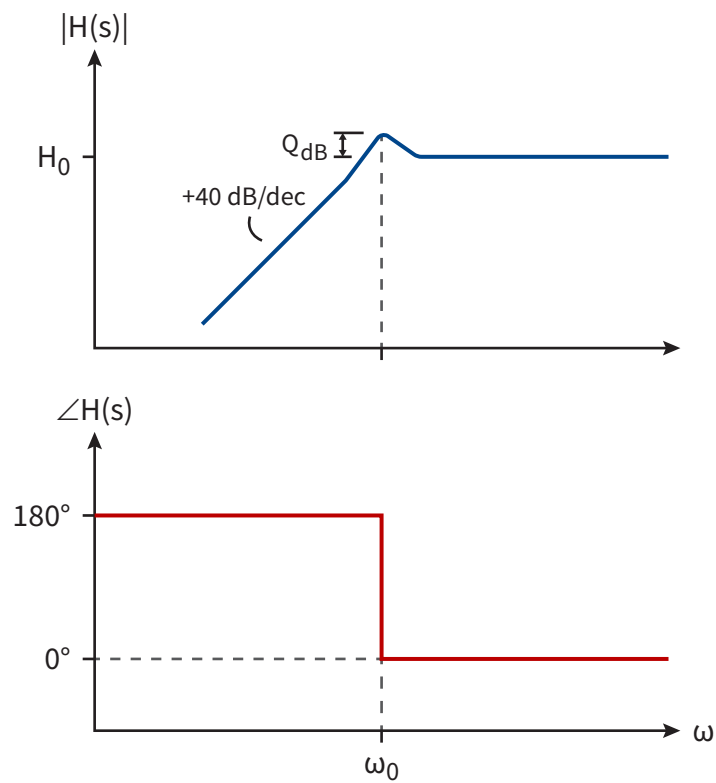


Figure 5: Sallen-Key high-pass filter Bode plot.

2.1 Sensitivity

$$S_{R_1}^{\omega_0} = S_{R_2}^{\omega_0} = S_{C_1}^{\omega_0} = S_{C_2}^{\omega_0} = -\frac{1}{2} \quad (32)$$

$$S_{R_B}^{\omega_0} = S_{R_A}^{\omega_0} = 0 \quad (33)$$

$$S_{R_2}^Q = -S_{R_1}^Q = \omega_0 Q (R_1 C_1 + R_1 C_2) - \frac{1}{2} \quad (34)$$

$$S_{C_2}^Q = -S_{C_1}^Q = \omega_0 Q R_1 C_1 - \frac{1}{2} \quad (35)$$

$$S_{R_B}^Q = -S_{R_A}^Q = \omega_0 Q (K - 1) R_2 C_2 \quad (36)$$

2.2 Components as Ratios

$$\begin{aligned} R_1 &= mR \\ R_2 &= R \\ C_1 &= nC \\ C_2 &= C \end{aligned} \quad (37)$$

$$\omega_0 = \frac{1}{RC\sqrt{mn}} \quad (38)$$

$$Q = \frac{\sqrt{mn}}{(1-K) + m(1+n)} \quad (39)$$

2.2.1 Minimizing Capacitor Sensitivity

$$S_{C_2}^Q = S_{C_1}^Q = 0 \text{ for}$$

$$\omega_0 Q R_1 C_1 = \frac{mn}{(1-K) + m(1+n)} = \frac{1}{2} \quad (40)$$

$$\Rightarrow n = \frac{(1-K) + m}{m} \quad (41)$$

Substituting n into Q and solving for m ,

$$m = \frac{1}{4Q^2} + (K-1) \quad (42)$$

$$\Rightarrow n = \frac{1}{1 + 4Q^2(K-1)} \quad (43)$$

If C is chosen, then R can be calculated from ω_0 as

$$R = \frac{2Q}{\omega_0 C} \quad (44)$$

2.2.2 Minimizing Resistor Sensitivity

$S_{R_2}^Q = S_{R_1}^Q = 0$ for

$$\omega_0 Q (R_1 C_1 + R_1 C_2) = \frac{m(1+n)}{(1-K) + m(1+n)} = \frac{1}{2} \quad (45)$$

However, the ratio expression has a minimum value of 1, so the minimum resistor sensitivity is $S_{R_2}^Q = -S_{R_1}^Q = 1/2$ and occurs when $K = 1$.

2.2.3 Monte Carlo Simulation

The circuit used to generate the plot was designed for $K = 1$, $\omega_0 = 2\pi \cdot 1000$, and $Q = 1.5$. The resistor and capacitor tolerances were set to 1% and 5%, respectively.

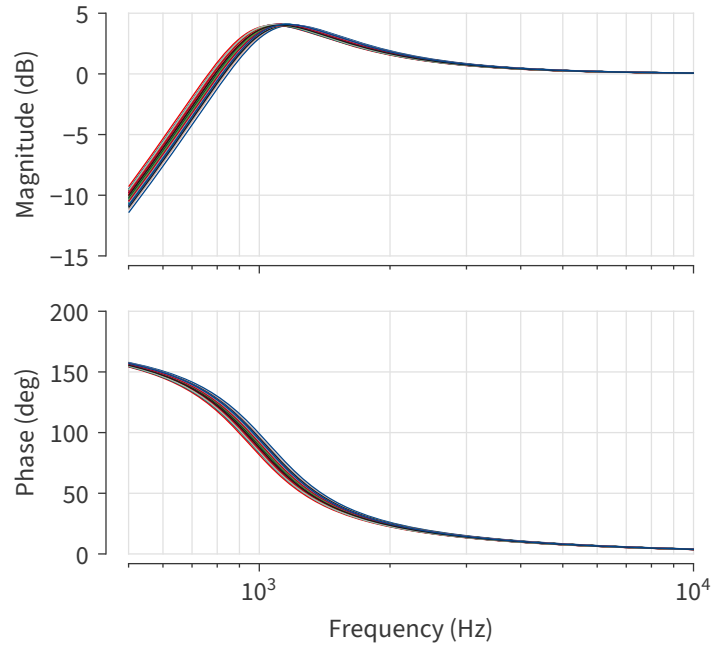


Figure 6: Sallen-Key high-pass filter Bode plot of 100 Monte Carlo samples.

2.3 Resistors as Ratios and Equal Capacitors

$$\begin{aligned}
 R_1 &= mR \\
 R_2 &= R \\
 C_1 &= C_2 = C
 \end{aligned}
 \tag{46}$$

$$\omega_0 = \frac{1}{RC\sqrt{m}}
 \tag{47}$$

$$Q = \frac{\sqrt{m}}{(1 - K) + 2m}
 \tag{48}$$

If C is chosen, then

$$m = \frac{\left[1 + \sqrt{1 + 8Q^2(K - 1)}\right]^2}{16Q^2} \quad (49)$$

$$R = \frac{4Q}{\left[1 + \sqrt{1 + 8Q^2(K - 1)}\right] \omega_0 C} \quad (50)$$

2.4 Equal Components

$$R_1 = R_2 = R \quad (51)$$

$$C_1 = C_2 = C$$

$$\omega_0 = \frac{1}{RC} \quad (52)$$

$$Q = \frac{1}{3 - K} \quad (53)$$

3 Band-Pass Filter

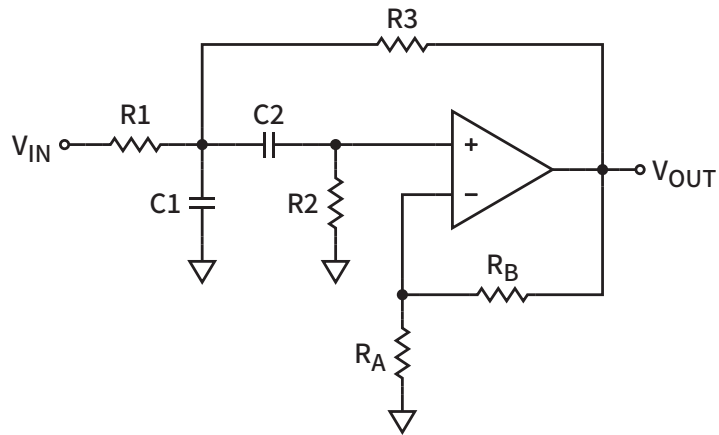


Figure 7: Sallen-Key band-pass filter schematic.

$$H(s) = H_0 \frac{s/(\omega_0 Q)}{s^2/\omega_0^2 + s/(\omega_0 Q) + 1} \quad (54)$$

$$K = 1 + R_B/R_A \quad (55)$$

$$H_0 = \frac{K}{1 + (1 - K) R_1/R_3 + (R_1/R_2) (1 + C_1/C_2)} \quad (56)$$

$$\omega_0 = \frac{\sqrt{1 + R_1/R_3}}{\sqrt{R_1 R_2 C_1 C_2}} \quad (57)$$

$$Q = \frac{\sqrt{1 + R_1/R_3} \cdot \sqrt{R_1 R_2 C_1 C_2}}{[1 + (1 - K) R_1/R_3] R_2 C_2 + R_1 (C_1 + C_2)} \quad (58)$$

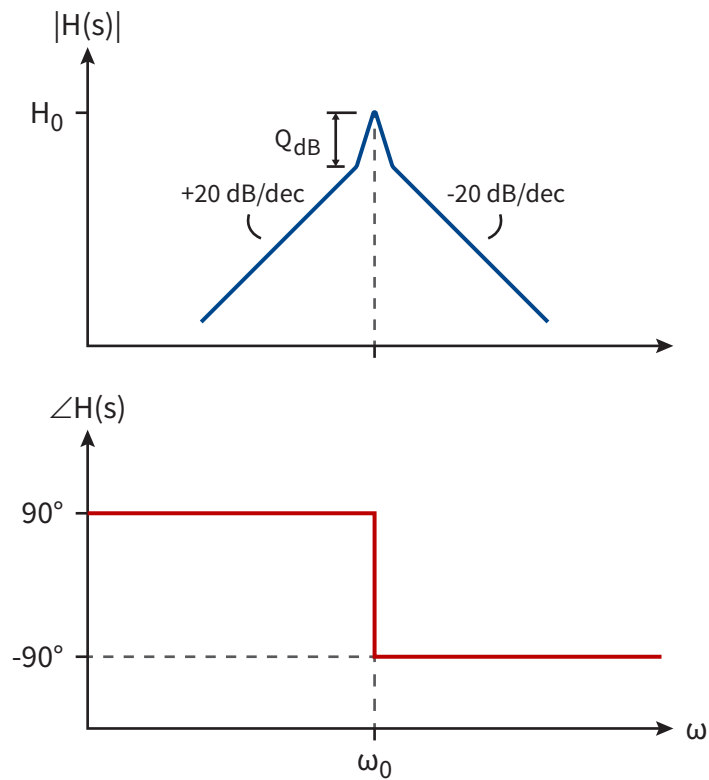


Figure 8: Sallen-Key band-pass filter Bode plot.

3.1 Sensitivity

$$S_{R_1}^{H_0} = \frac{H_0}{K} - 1 \quad (59)$$

$$S_{R_2}^{H_0} = \frac{H_0}{K} \cdot \frac{R_1}{R_2} \left(1 + \frac{C_1}{C_2}\right) \quad (60)$$

$$S_{R_3}^{H_0} = \frac{H_0}{K} \cdot \frac{R_1}{R_3} (1 - K) \quad (61)$$

$$S_{C_2}^{H_0} = -S_{C_1}^{H_0} = \frac{H_0}{K} \cdot \frac{R_1 C_1}{R_2 C_2} \quad (62)$$

$$S_{R_B}^{H_0} = -S_{R_A}^{H_0} = \left(H_0 \frac{R_1}{R_3} + 1\right) \frac{K - 1}{K} \quad (63)$$

$$S_{R_1}^{\omega_0} = -\frac{R_3}{2(R_1 + R_3)} \quad (64)$$

$$S_{R_2}^{\omega_0} = S_{C_1}^{\omega_0} = S_{C_2}^{\omega_0} = -\frac{1}{2} \quad (65)$$

$$S_{R_3}^{\omega_0} = -\frac{R_1}{2(R_1 + R_3)} \quad (66)$$

$$S_{R_B}^{\omega_0} = S_{R_A}^{\omega_0} = 0 \quad (67)$$

$$S_{R_1}^Q = S_{R_1}^{H_0} + S_{R_1}^{\omega_0} + 1 \quad (68)$$

$$S_{R_2}^Q = S_{R_2}^{H_0} + S_{R_2}^{\omega_0} \quad (69)$$

$$S_{R_3}^Q = S_{R_3}^{H_0} + S_{R_3}^{\omega_0} \quad (70)$$

$$S_{C_2}^Q = -S_{C_1}^Q = S_{C_2}^{H_0} + S_{C_2}^{\omega_0} \quad (71)$$

$$S_{R_B}^Q = -S_{R_A}^Q = S_{R_B}^{H_0} + S_{R_B}^{\omega_0} - \frac{K - 1}{K} \quad (72)$$

3.2 Components as Ratios

$$R_1 = mR$$

$$R_2 = nR$$

$$R_3 = R \quad (73)$$

$$C_1 = oC$$

$$C_2 = C$$

$$H_0 = \frac{K}{1 + (1 - K)m + (1 + o)m/n} \quad (74)$$

$$\omega_0 = \frac{\sqrt{1 + m}}{RC\sqrt{mno}} \quad (75)$$

$$Q = \frac{\sqrt{1 + m} \cdot \sqrt{mno}}{[1 + (1 - K)m]n + m(1 + o)} \quad (76)$$

3.2.1 Minimizing Resistor and Capacitor Sensitivities

$$S_{R_1}^Q = \frac{1}{1 + (1 - K)m + (1 + o)m/n} - \frac{1}{2(1 + m)} \quad (77)$$

$$S_{R_2}^Q = \frac{(1 + o)m/n}{1 + (1 - K)m + (1 + o)m/n} - \frac{1}{2} \quad (78)$$

$$S_{R_3}^Q = \frac{(1 - K)m}{1 + (1 - K)m + (1 + o)m/n} - \frac{m}{2(1 + m)} \quad (79)$$

$$S_{C_2}^Q = -S_{C_1}^Q = \frac{mo/n}{1 + (1 - K)m + (1 + o)m/n} - \frac{1}{2} \quad (80)$$

Minimizing the component sensitivities is more easily solved numerically with constraints set on the upper and lower bounds of the component ratios.

If C is chosen, then R can be calculated from ω_0 as

$$R = \frac{\sqrt{1 + m}}{\omega_0 C \sqrt{mno}} \quad (81)$$

3.2.2 Example MATLAB Script

```

1  %% Specifications
2
3  K = 1;
4  H0 = 0.5;
5  w0 = 2*pi*1e3;
6  Q = 1.5;
7  C = 10e-9;
8

```

```

9 %% Sensitivity optimization
10
11 x0 = ones(1, 3); % Initial values for m, n, and o
12 lb = 0.01 * ones(1, length(x0)); % Lower bound
13 ub = 100 * ones(1, length(x0)); % Upper bound
14
15 fun_wrapper = @(x) fun(x, K);
16 nonlcon_wrapper = @(x) nonlcon(x, K, H0, Q);
17 [x, fval] = fmincon(fun_wrapper, x0, [], [], [], [],
    lb, ub, nonlcon_wrapper);
18
19 m = x(1);
20 n = x(2);
21 o = x(3);
22 R = sqrt(1 + m)/(w0*C*sqrt(m*n*o));
23
24 %% Functions
25
26 function f = fun(x, K)
27     m = x(1);
28     n = x(2);
29     o = x(3);
30
31     H0_K = 1/(1 + (1 - K)*m + (1 + o)*m/n);
32     S_Q_R1 = H0_K - 1/(2*(1 + m));
33     S_Q_R2 = H0_K*((1 + o)*m/n) - 1/2;
34     S_Q_R3 = H0_K*((1 - K)*m) - m/(2*(1 + m));
35     S_Q_C2 = H0_K*(m*o/n) - 1/2;
36     S_Q_C1 = -S_Q_C2;
37
38     % Sum of all the absolute sensitivities to be
39     % minimized
40     f = abs(S_Q_R1) + abs(S_Q_R2) + abs(S_Q_R3) + abs
41         (S_Q_C1) + abs(S_Q_C2);
42 end
43
44 function [c, ceq] = nonlcon(x, K, H0, Q)
45     m = x(1);
46     n = x(2);
47     o = x(3);

```

```

46
47     c = [];
48
49     % Constrain the parameters to meet the specified
      H0 and Q
50     ceq(1) = H0 - K/(1 + (1 - K)*m + (1 + o)*m/n);
51     ceq(2) = Q - (sqrt(1 + m)*sqrt(m*n*o))/((1 + (1 -
      K)*m)*n + (1 + o)*m);
52 end

```

3.2.3 Monte Carlo Simulation

The circuit used to generate the plot was designed for $K = 1$, $H_0 = 0.5$, $\omega_0 = 2\pi \cdot 1000$, and $Q = 1.5$. The resistor and capacitor tolerances were set to 1% and 5%, respectively.

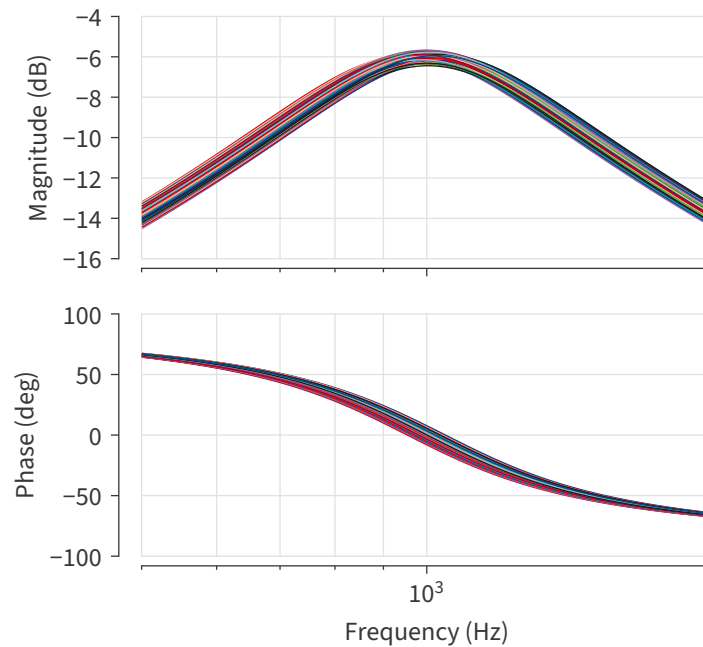


Figure 9: Sallen-Key band-pass filter Bode plot of 100 Monte Carlo samples.

3.3 Equal Capacitors and $K = 1$

$$\begin{aligned} C_1 = C_2 = C \\ K = 1 \end{aligned} \quad (82)$$

$$H_0 = \frac{1}{1 + 2R_1/R_2} \quad (83)$$

$$\omega_0 = \frac{\sqrt{1 + R_1/R_3}}{C\sqrt{R_1R_2}} \quad (84)$$

$$Q = \frac{\sqrt{1 + R_1/R_3} \cdot \sqrt{R_1R_2}}{2R_1 + R_2} \quad (85)$$

If C is chosen, then

$$R_1 = \frac{Q}{H_0\omega_0C} \quad (86)$$

$$R_2 = \frac{2Q}{(1 - H_0)\omega_0C} \quad (87)$$

$$R_3 = \frac{(1 - H_0)Q}{(H_0^2 - H_0 + 2Q^2)\omega_0C} \quad (88)$$

3.4 Equal Components

$$\begin{aligned} R_1 = R_2 = R_3 = R \\ C_1 = C_2 = C \end{aligned} \quad (89)$$

$$H_0 = \frac{K}{4 - K} \quad (90)$$

$$\omega_0 = \frac{\sqrt{2}}{RC} \quad (91)$$

$$Q = \frac{\sqrt{2}}{4 - K} \quad (92)$$

References

- [1] S. Franco, *Design with Operational Amplifiers and Analog Integrated Circuits*, 4th ed. McGraw Hill, 2015, ISBN: 978-0-07-802816-8.
- [2] L. P. Huelsman and P. E. Allen, *Introduction to the Theory and Design of Active Filters*. McGraw Hill, 1980, ISBN: 978-0-07-030854-1.
- [3] Maxim Integrated, "Minimizing Component-Variation Sensitivity in Single Op Amp Filters," Application Note 738, Jul. 22, 2002.
- [4] Texas Instruments, "OA-28 Low-Sensitivity, Bandpass Filter Design With Tuning Method," Application Note SNOA373C, Apr. 2013.